

How to Cite:

de Gayo, F. (2019). Brake performance is evaluated by the varying pedal ratios. *Tennessee Research International of Social Sciences*, 1(1), 52–62. Retrieved from <https://triss.org/index.php/journal/article/view/11>

Brake performance is evaluated by the varying pedal ratios

Francisco de Gayo

University of Barcelona, Barcelona, Spain

Abstract---The proper pedal design work also determines the size of the master cylinder to be adopted for the vehicle. Depending on the pedal ratio the work can be extended for the study of pedal travel. Brake performance is evaluated by the varying pedal ratios and pedal force other than the standard ratio a slight variation which resulted in the ratio gives more sustainable results under respective load conditions. As described in the above work a very slight variation in the pedal ratios show a large variation in the braking forces. Therefore by maintaining proper pedal ratios, the length of the pedal can be made compact and with effective braking effects. This phenomenon is useful in the case of racing vehicles as it reduces the effort of the driver.

Keywords---Performance, Pedal, Vehicle, Society, Braking forces.

Introduction

A brake is a Mechanical element utilizing which artificial frictional resistance is applied to the moving elements, to stop the motion of the machine, the present work aims in optimizing the Brake performance by changing the Pedal ratios and applied Pedal force. In this paper, a Brake disc is designed in Solid Works and the analysis of the disc is done in ANSYS by varying pedal ratios and pedal forces. Therefore the main aim of this paper is to evaluate the brake performance by determining an optimum pedal ratio for easiness and flexibility of the driver. Generally, the Disc used in the brake system is made of grey cast iron casting after proper design. Most of the automobile shops will not respond for disc problems often they used to replace the brake system, this is done where the service cost is more than the replacement cost but as per mechanical design, Most of the brake discs are made of gray cast iron, so discs are damaged in one of three ways Scoring, cracking, Warping or excessive rusting and the type of forces acting on the brake disc. The deformation or any sorts of stress are developed on the disc after the application of the forces. There are two types of forces are acting on the brake pedal, the general tangential force is defined as the force which is acting on a moving body in the perpendicular direction to the motion of the body,

Tennessee research international of social sciences © 2019.

ISSN: 2766-7464 (Online)

Publisher: Smoky Mountain Publishing

Manuscript submitted: 09 March 2019, Manuscript revised: 18 April 2019, Accepted for publication: 27 May 2019

with this effect the velocity may increase or decrease. Tangential force (T.F) is used to determine the stress developed in discs. The tangential force is the product of the frictional coefficient and caliper force.

Another force is clamping force which is defined as the force pressing each brake pad against the disc and is the product of brake pressure; area of caliper piston and the number of pistons, the brake pressure is the ratio of the force on the brake pedal and the area of the master cylinder. Different forces acting on a disc brake is shown in figure1. The braking pressure is the tangential friction force acting between the brake pads and disc, which is calculated by the product of the force applied by the driver and pedal ratio. The Braking torque is the moment of a braking force about the center of rotation, which is calculated by the product of tangential force and radius of the disc. Another parameter is stopping distance which is the distance moved between the instant when the rider decides to retard the vehicle moving, and the instant when the vehicle comes to rest. In general, the stopping distance is depending on factors, like road conditions i.e. rough or smooth (coefficient of friction), and the driving skills of the driver. As the work done by the brake is equal to the kinetic energy loosed by the vehicle during that time the heat dissipated to the surroundings all are equal, means the vehicle loses the kinetic energy and work done on the brake by equating the work done by the brake and lose of kinetic energy the stopping distance can be calculated.

$$\text{Tangential force} \times \text{Distance travelled} = \frac{1}{2}mv^2 (\text{Kinetic energy})$$

The factors which are responsible for brake performance are change in pedal ratio, change of driver applied force on the pedal, change in dimensions i.e., diameter of the disc brake, change in velocity of the vehicle, change in material properties. From these reasons we have considered the variations in the pedal ratio and relatively the changes in the driver applied force on pedal to determine the deformations occurring and thus the brake performance.

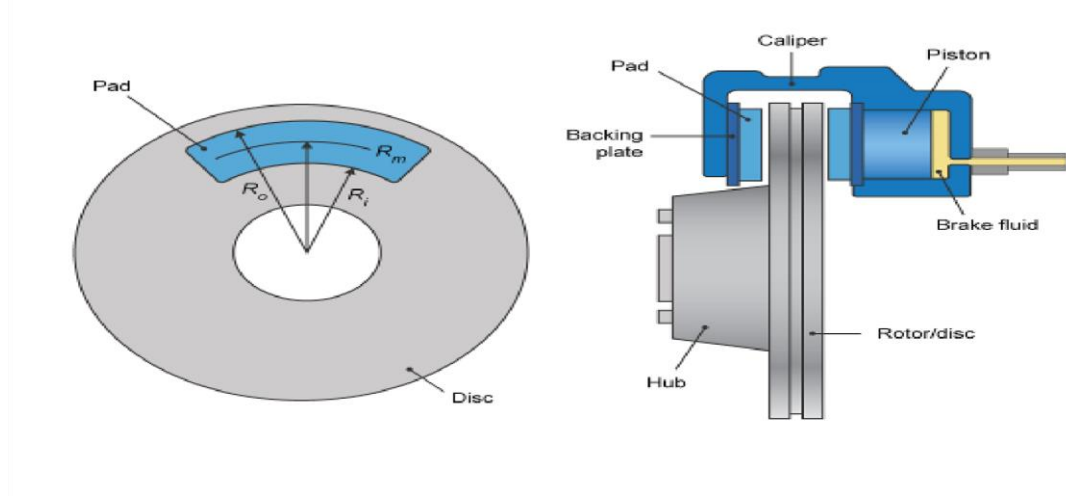


Figure 1: Forces acting on a braking system

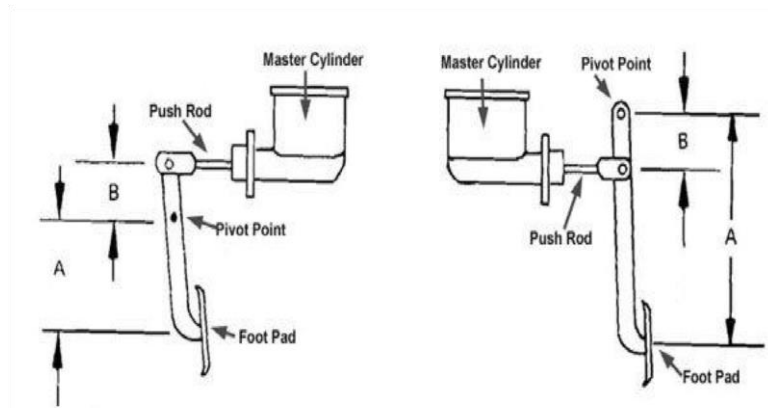


Figure 2: Different pedal alignments

About Pedal Ratio

In this work three different conditions are tested for go-kart vehicle based on the different leverage principles mainly first or second lever principles are adopted in designing the brake pedal. Brake pedal multiplies the force exerted by the driver on pedal. Brake pedal alignments are done based on first or second lever principles. Pedal ratio is the ratio of leverage your clutch pedal applies to the master cylinder. To determine the pedal ratio you need to measure the height of the pedal to the pivot point then divided the measurement of the pivot point to the lower arm that controls your rod to the master cylinder. When a brake pedal gets modified to “fit” in a vehicle or a booster/master cylinder gets installed where it “fits” in the car, the pedal ratio is rarely taken into consideration. Proper pedal ratio is a must when installing and operating a brake system. Below in fig3 shows how to properly figure pedal ratio:

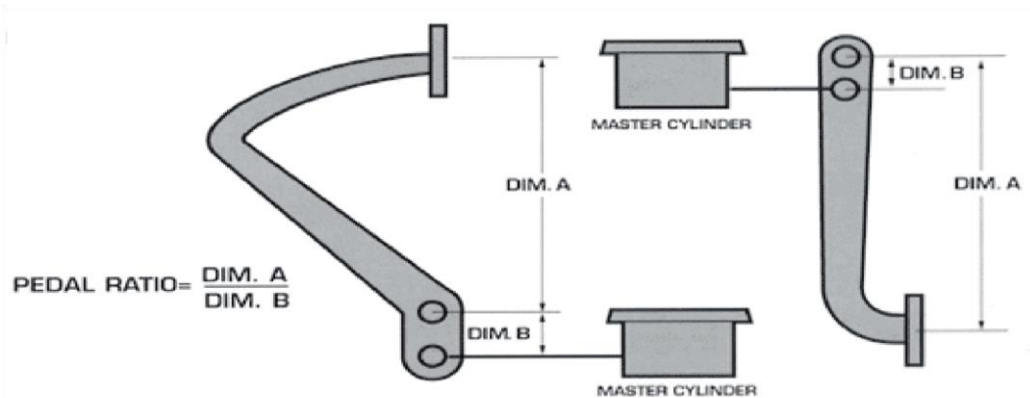


Figure 3: Brake pedal ratio

In a manual brake system, the pedal ratio will be between 5:1 and 6:1 and a power brake system it will be between 4:1 and 5:1. An excellent example is our Mustang kits for the 1967-1970 years. We include a brake pedal to adjust the ratio from the manual ratio to the desired power ratio. The new pedal raises the

upper mounting pivot point about 2 ½". If the correct pedal ratio is not achieved, the pedal will be extremely sensitive due to too much pressure being applied too quickly.

How to Measure Brake Pedal Ratio

When the brake pedal (or clutch pedal) is too hard to push, driving your car becomes not only difficult, but downright dangerous. Disc brake conversions are great, but even converting to a power-assist braking system can alter the feel of the brake pedal, and not all vehicles are capable of using power brakes, so ensuring that the pedal ratio is correct is paramount to practical and safe operation of the vehicle. This is a common theme for customized cars, one that is too often ignored.

A common misunderstanding with master cylinders is selecting the right one. The main issue with manual brake master cylinders is that the larger the cylinder bore, the harder it is to press. This is due to the fact that there is more fluid in front of it. The rule of thumb for manual brakes is no larger than 1", with 7/8" being optimum for factory-type master cylinders. Power-assist master cylinders have a lot of help to move that piston, so they use a larger cylinder bore. Do not use a power master cylinder in a manual application.

The master cylinder bore size is a key component to getting functional brakes. Even with the correct master cylinder, the brake pedal ratio is the biggest factor in pedal effort. Pedal ratio difference in length between the pivot (fulcrum) of the pedal to the pushrod hole (Y) and the fulcrum to the center of the brake pedal (X). A power system should have a ratio between 4 and 5:1, where a manual system should be between 5 and 7:1. Master cylinder with a 1-inch bore and a brake pedal ratio of 6:1 with 100 pounds of pedal pressure yields 600 pounds of pressure at the master cylinder. Cut that brake pedal ratio to 4:1, and the pressure at the master drops to just 400 pounds with the same effort, that is a significant difference.

Testing and Analysis

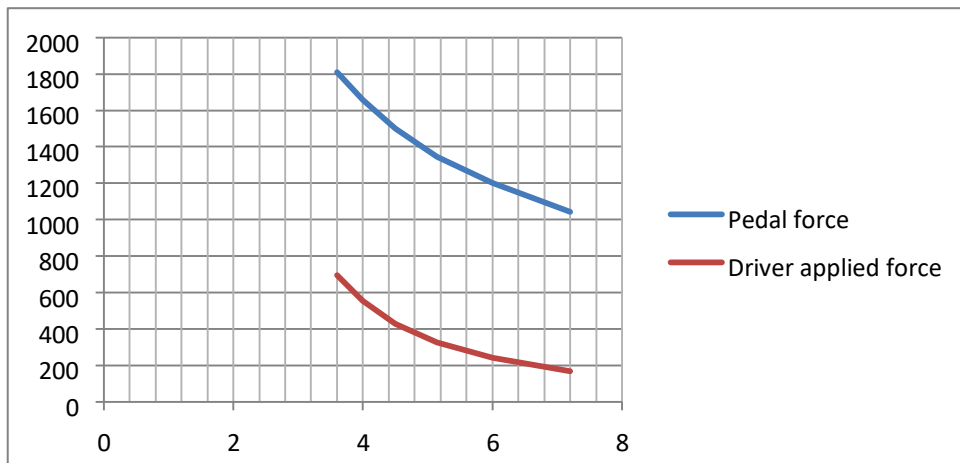
In this work different cases are considered based on the literature and overall length(A+B) ("A" represents distance between pivot to master cylinder and B indicates the distance between pivot rod to push rod as shown in fig 2) is considered as 18 cm as most of the go karts will use this pedal ratio. The following parameters are considered for the pedal force calculation; these values are taken from the go-kart system developed in our institution. The pedal force calculations are done by assuming no slip occurs in the brake and the frictional coefficient as 0.4 as the pedal contains rubber pad, with this anyone can alter the value of Frictional coefficient.

Parameters	Values
Frictional coefficient	0.4
Master cylinder diameter	10mm
Caliper piston diameter	25.4mm
No. of calipers used	02
Velocity	45km/hr
Pedal length	18cm

Theoretical Output

No	Total length of brake pedal(A+B)	Length (A)	Length (B)	Pedal ratio(A+B/B)	Pedal Force N
1	18	15.5	2.5	7.2	1042
2	18	15	3	6.0	1200
3	18	14.5	3.5	5.1	1345
4	18	14	4	4.5	1500
5	18	13.5	4.5	4.0	1658
6	18	13	5	3.6	1810

No	Pedal ratio	Pedal force	Driver applied force
1	7.2	1042	168.1
2	6.0	1200	240.0
3	5.1	1345	324.7
4	4.5	1500	428.6
5	4.0	1658	552.7
6	3.6	1810	696.2



Graph 1: Variation of driver applied force with pedal force

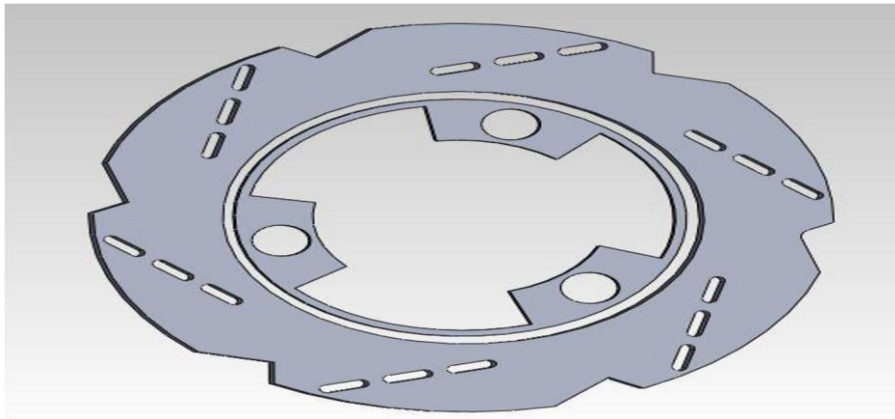
Modeling Analysis of Disc

From the above graphs it is clear that a slight variation in the pedal ratio resulted in large variation in the clamping forces and stopping distances a 200 mm diameter disc is used for the design and analysis of brakes performance. For the above mentioned diameter the deformations and stress conditions are determined. Along with dimensions the material properties are important to verify its performance. The material of disc being used is GREY CAST IRON Grey cast iron is the traditional material used for brake disc applications for the majority of the vehicles. Grey cast iron offers superior properties and advantages, and is more suited to brake disc manufacture when compared to other irons such as ductile (SG) iron and compacted graphite cast iron. The primary advantage of this grey cast iron is its high thermal conductivity, arising from continuous flake graphite structure, giving the brake disc the ability to dissipate heat efficiently, which is essential for the intended applications.

Grey Cast Iron Disc Material Properties

PROPERTIES	VALUES
Density	7200kg/m ³
Young's Modulus	110Gpa
Poisson's ratio	0.28
Thermal conductivity	53.3-54

Based on the above theoretical conclusions and material properties, a brake disc has been designed for go-kart

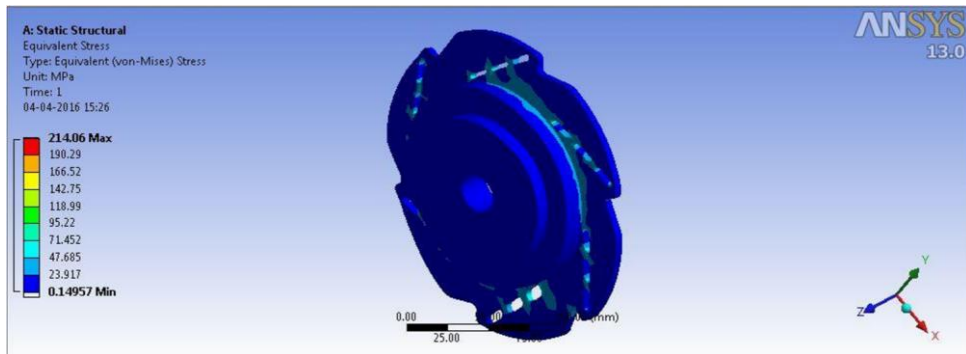


Analysis of the Disc

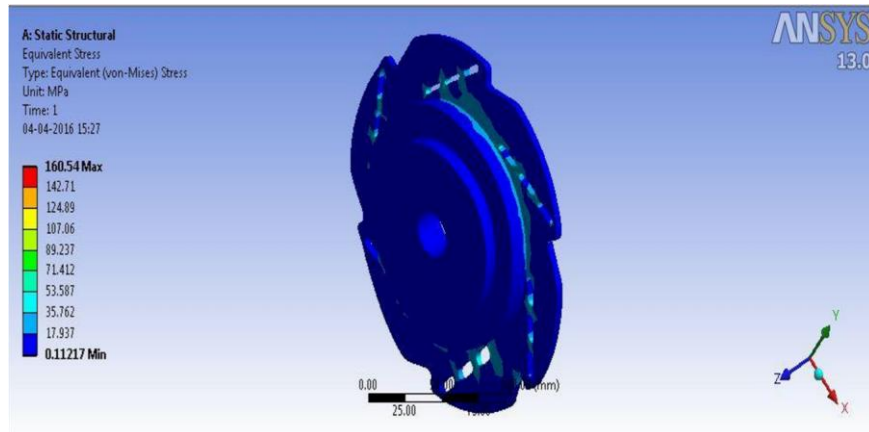
Final considerations which are made for the analysis of the disc Since the material used is grey cast iron, we have it's Material Properties and it's respective values as- Ultimate tensile strength of grey cast iron as 140-145Mpa and Yield Strength as 98-276Mpa. Factor of Safety (FOS): In a static structural analysis, FOS value ranges between 2 to 3. If the FOS value is below or above the range,

the disc cannot sustain for the given pedal force and pedal ratio. The braking force which is obtained for different pedal ratios and pedal forces applied is tabulated as given below. The disc is analyzed for the following pedal forces and pedal ratios based on that the tangential force is calculated.

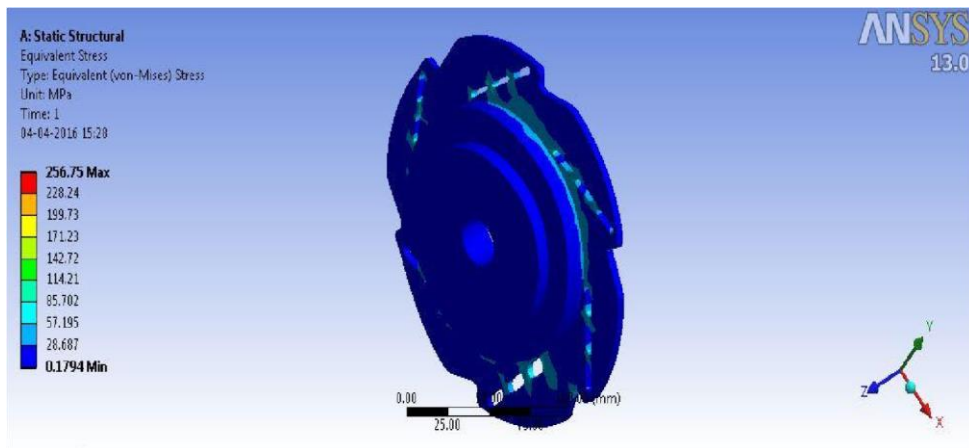
Based on the above values and calculations, the results obtained in ANSYS are
CASE 1: Pedal force=1200N, pedal ratio=6:1, Braking Force=35996.72N; FOS=2.1



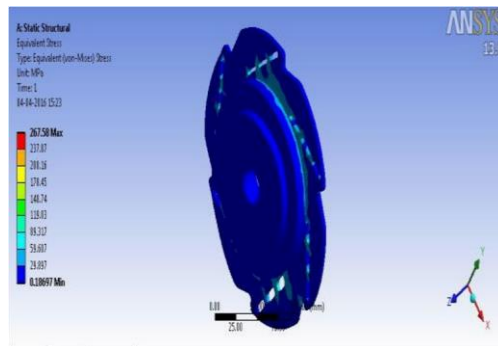
CASE 2: Pedal force=1200N, pedal ratio=4.5:1, Braking Force=26336.06N; FOS=2.8



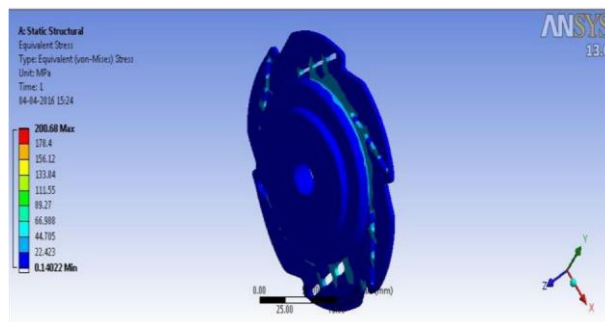
CASE 3: Pedal force=1200N, Pedal ratio=4.5:0.625, Braking Force=46175.89N; FOS=1.75



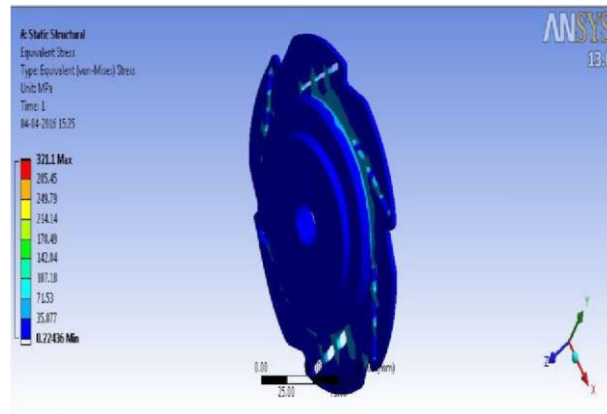
CASE 4: Pedal force=1500N, Pedal ratio=6:1, Braking Force=44996.04N;
FOS=1.68



CASE 5: Pedal force=1500N, Pedal ratio=4.5:1, Braking Force=33747.84N;
FOS=2.2



CASE 6: Pedal force=1500N, Pedal ratio=4.5:0.625, Braking Force=53996.223N
FOS=1.40



Comparing the FOS obtained for different Pedal forces and Pedal Ratios FOS obtained for different cases

Pedal forces	Pedal ratios	Factor Of Safety(FOS)
1200N	7.2	2.1
1200N	4.5	2.8
1200N	3.6	1.75
1500N	7.2	1.68
1500N	4.5	2.2
1500N	3.6	1.40

Conclusion

The brake disc having a factor of safety (FOS) within the range of 2 to 3 is sustainable. The disc with a FOS less than 2 or greater than 3 undergoes distortion and are less sustainable. Theoretically it has been proven using graphs and calculations that a slight variation in the pedal ratio leads to a large variation in the clamping forces and stopping distance. As per the analysis, factor of safety is the basic criteria that determine the sustainability of the disc.

When the structure is said to be steady, the Factor of Safety (FOS) ranges between 2 – 3. As per the comparisons made from the FOS and as per result from ANSYS, when the pedal force is 1200N and the pedal ratios are 7.2 and 4.5, the FOS are 2.1 and 2.8 respectively. Hence the disc is sustainable. When the pedal force is 1500N, and the pedal ratio is 4.5, the FOS is 2.2. Hence in this case too, the disc is sustainable.

Hence, as the Brake performance is evaluated by the varying pedal ratios and pedal force other than standard ratio a slight variation which resulted in the ratio gives more sustainable results under respective load conditions. As described in the above work a very slight variation in the pedal ratios show a large variation in the braking forces. Therefore by maintaining proper pedal ratios, the length of the pedal can be made compact and with effective braking effects. This phenomenon is useful in case of racing vehicles as it reduces the effort of driver. The proper pedal design work also determines the size of master cylinder to be

adopted for the vehicle. Depending on pedal ratio the work can be extended for study of pedal travel.

References

- Chase, T. P. (1949). Passenger-Car Brake Performance Limitations and Future Requirements (No. 490175). SAE Technical Paper.
- D'alfio, N., Morgando, A., & Sorniotti, A. (2006). Electro-hydraulic brake systems: design and test through hardware-in-the-loop simulation. *Vehicle System Dynamics*, 44(sup1), 378-392.
- de Groot, S., de Winter, J. C., Mulder, M., & Wieringa, P. A. (2011). Car racing in a simulator: Validation and assessment of brake pedal stiffness. *Presence: Teleoperators and Virtual Environments*, 20(1), 47-61.
- De Rosario, H., Louredo, M., Díaz, I., Soler, A., Gil, J. J., Solaz, J. S., & Jornet, J. (2010). Efficacy and feeling of a vibrotactile Frontal Collision Warning implemented in a haptic pedal. *Transportation research part F: traffic psychology and behaviour*, 13(2), 80-91.
- Freund, B., Colgrove, L. A., Petrakos, D., & McLeod, R. (2008). In my car the brake is on the right: Pedal errors among older drivers. *Accident Analysis & Prevention*, 40(1), 403-409.
- Godfrey, A. J., & Sankaranarayanan, V. (2018). A new electric braking system with energy regeneration for a BLDC motor driven electric vehicle. *Engineering Science and Technology, an International Journal*, 21(4), 704-713.
- He, R., Liu, X., & Liu, C. (2013). Brake performance analysis of ABS for eddy current and electrohydraulic hybrid brake system. *Mathematical Problems in Engineering*, 2013.
- Johnston, M., Leonard, E., Monsere, P., & Riefe, M. (2005). *Vehicle brake performance assessment using subsystem testing and modeling* (No. 2005-01-0791). SAE Technical Paper.
- Kumar, C. N., & Subramanian, S. C. (2016). Cooperative control of regenerative braking and friction braking for a hybrid electric vehicle. *Proceedings of the Institution of Mechanical Engineers, Part D: Journal of Automobile Engineering*, 230(1), 103-116.
- Lee, C. H., Lee, J. M., Choi, M. S., Kim, C. K., & Koh, E. B. (2011). Development of a semi-empirical program for predicting the braking performance of a passenger vehicle. *International Journal of Automotive Technology*, 12(2), 193-198.
- Lee, H., & Kim, H. (2005). Improvement in fuel economy for a parallel hybrid electric vehicle by continuously variable transmission ratio control. *Proceedings of the Institution of Mechanical Engineers, Part D: Journal of Automobile Engineering*, 219(1), 43-51.
- Leiber, H. (1987). *U.S. Patent No. 4,678,243*. Washington, DC: U.S. Patent and Trademark Office.
- Lotte, J. S., Luuk, D. S., Max, S. N., & Nick, A. S. (2019). The brake pressure depends upon the pedal ratio. *International research journal of management, IT and social sciences*, 6(6), 178-187.
- Moosavi-Rad, H., & Ullman, D. G. (1990). A band variable-inertia flywheel integrated-urban transit bus performance. *SAE transactions*, 933-942.

- Naseri, F., Farjah, E., & Ghanbari, T. (2016). An efficient regenerative braking system based on battery/supercapacitor for electric, hybrid, and plug-in hybrid electric vehicles with BLDC motor. *IEEE Transactions on Vehicular Technology*, 66(5), 3724-3738.
- Park, E. J., Stoikov, D., da Luz, L. F., & Suleman, A. (2006). A performance evaluation of an automotive magnetorheological brake design with a sliding mode controller. *Mechatronics*, 16(7), 405-416.
- Park, S., & Sheridan, T. B. (2004). Enhanced human-machine interface in braking. *IEEE Transactions on Systems, Man, and Cybernetics-Part A: systems and humans*, 34(5), 615-629.
- Park, S., Bae, S., & Lee, J. M. (2005). Numerical evaluation of braking feel to design optimal brake-bywire system. *International journal of vehicle design*, 37(1), 1-23.
- Pereira, J. A. D. A. (2003). *New Fiesta: brake pedal feeling development to improve customer satisfaction* (No. 2003-01-3598). SAE Technical Paper.
- Petrucelli, L., Velardocchia, M., & Sorniotti, A. (2003). *Electro-hydraulic braking system modelling and simulation* (No. 2003-01-3336). SAE Technical Paper.
- Reuter, D. F., Lloyd, E. W., Zehnder, J. W., & Elliott, J. A. (2003). *Hydraulic design considerations for EHB systems* (No. 2003-01-0324). SAE Technical Paper.
- Sangtarash, F., Esfahanian, V., Nehzati, H., Haddadi, S., Bavanpour, M. A., & Haghpanah, B. (2009). Effect of different regenerative braking strategies on braking performance and fuel economy in a hybrid electric bus employing CRUISE vehicle simulation. *SAE International Journal of Fuels and Lubricants*, 1(1), 828-837.
- Segel, L., & Mortimer, R. (1970). *Driver braking performance as a function of pedal-force and pedaldisplacement levels* (No. 700364). SAE Technical Paper.
- Song, J. (2005). Performance evaluation of a hybrid electric brake system with a sliding mode controller. *Mechatronics*, 15(3), 339-358.
- Sorniotti, A. (2006). *Virtual and experimental analysis of brake assist systems* (No. 2006-01-0477). SAE Technical Paper.
- Wang, B., Huang, X., Wang, J., Guo, X., & Zhu, X. (2015). A robust wheel slip ratio control design combining hydraulic and regenerative braking systems for in-wheel-motors-driven electric vehicles. *Journal of the Franklin Institute*, 352(2), 577-602.
- Yun, D., Kim, H., & Boo, K. (2011). Brake performance evaluation of ABS with sliding mode controller on a split road with driver model. *International Journal of Precision Engineering and Manufacturing*, 12(1), 31-38.
- Zehnder, J. W., Kanetkar, S. S., & Osterday, C. A. (1999). Variable rate pedal feel emulator designs for a brake-by-wire system. *SAE transactions*, 881-884.
- Zhao, D., Chu, L., Xu, N., Sun, C., & Xu, Y. (2018). Development of a cooperative braking system for front-wheel drive electric vehicles. *Energies*, 11(2), 378.
- Zulhilmi, I. M., Peeie, M. H., Eiman, R. I. M., Izhar, I. M., & Asyraf, S. M. (2019). Investigation on vehicle dynamic behaviour during emergency braking at different speed. *International Journal of Automotive and Mechanical Engineering*, 16(1), 6161-6172.